Corrosion Behavior of Ni/Al₂O₃ and Ni/ZrO₂ Nanocomposite Thin Films

Gheorghies Constantin¹, Stasi Iuliana-Valentina² and Lalau Cornel-Constantin¹

¹“Dunarea de Jos” University of Galati
²S.C. Automobile DACIA S.A. Pitesti
Romania

1. Introduction

This paper investigates the effects of adding alumina and zirconia nanoparticles in the electrolyte bath on surface morphologies and structure of electrodeposited nickel, and their subsequent influence on the corrosion process in various solutions. These results are important for the fabrication of thermal and corrosion barriers by means of covering metallic surfaces with protective layers.

2. Nanocomposite preparation

The electrodeposition process and corrosion studies have been preformed on the same electrochemical cell. The corrosion process was monitored in a corrosion cell consisting of a round-bottomed flask, platinum auxiliary electrodes, and a standard calomel electrode serving as the reference electrode. The applied potential and resulting current were measured by a VOLTALAB 10 and 80 potentiostat/galvanostat and with a typical corrosion measurement software from RADIOMETER ANALYTICAL SAS Company. The general view of experimental arrangement is shown in figure 1. The temperature of the used solutions was controlled when placing the electrochemical cell in MLW U7 C thermostat.

On copper support, we have deposited 10 nanocomposite layers, in a nickel matrix, with ZrO₂ particles (6-8 nm) and 7 specimens having similar matrix with Al₂O₃ particles (20 nm) (Abreu et al., 2006; Yoo et al., 2006). We also created 3 specimens with simple nickel deposition in order to compare their behavior with the version with nanoparticles. The support specimens have been properly prepared for deposition, using specific solutions for degreasing, pickling and activation of surfaces. For the electrolyte solution, a Watt bath was used having the following features: NiSO₄·6H₂O-0.90M; NiCl₂·6H₂O-0.20M; H₃BO₃-0.28M; sodium dodecylsulphate [CH₃(CH₂)₁₁OSO₃Na]-0.4 g/l (Viswanathan et al., 2006). The pH value of the solution was maintained at 4.2 – 4.5 and the corrections were made using an acidic solution. The concentration of zirconia was 10 g/l and concentration of alumina varied from 0 to 20 g/L. Both types of nanoparticles were kept in suspension by a magnetic stirrer. The stirring rate of the plate agitator was 700 rpm. Firstly, the supports are decreased for 15-20 minutes in a solution and then wiped with a filter paper. Secondly, the specimen is introduced in the pickling solution (HNO₃ 20%) and thoroughly rinsed distilled water. We
noticed that the surface shows metallic lustre and the wash with distilled water creates a uniform film. Thirdly, the specimen is introduced in an activating solution (H₂SO₄ 50%) and washed again with distilled water. Finally, it is rapidly introduced in the electrolysis bath containing the prepared electrolyte solution. Before weighting them on a precision balance, the specimens need to be thoroughly dried. Depositions were made at an optimal temperature of 40°C for 90 minutes and a current density of 2A/dm². The cathode consisted of the working specimen and the anode consisted of pure nickel with the same surface area as the specimen. After 90 minutes, the electric power was disconnected and electrodes were removed from the bath. The specimens with composite deposition were washed with plenty of distilled water. After the specimens dries, they are weighed on the precision balance to compute the actual deposited quantity.

The main tools used for the surface characterization for nanocomposite layers were scanning electron microscopy (SEM) equipped with an EDAX, and X-ray diffractometer (XRD). The OLYMPUS PM3 microscope allows for morphological observations of the microstructure. The analysis by XRD shows that only some planes common to nickel system are expected and these are presented in Table 1.

<table>
<thead>
<tr>
<th>(hkl)</th>
<th>2θ (°)</th>
<th>I (a.u.)</th>
</tr>
</thead>
<tbody>
<tr>
<td>111</td>
<td>44.51</td>
<td>100</td>
</tr>
<tr>
<td>200</td>
<td>51.85</td>
<td>42</td>
</tr>
<tr>
<td>220</td>
<td>76.37</td>
<td>21</td>
</tr>
<tr>
<td>311</td>
<td>92.94</td>
<td>20</td>
</tr>
</tbody>
</table>

Table 1. Planes of nickel system

3. Structural analysis

The obtained electrodeposited layers of nickel having alumina or zirconia nanoparticles were studied by scanning electron microscopy at different magnifications. It is important to choose the optimal magnifications to obtain the best images in which some agglomeration of nanoparticles in the electrodeposited layers can be observed.
If a cross section is made in the resulted nanomaterial, it is possible to observe different thicknesses of the electrodeposited layer. This thickness depends of current density, the deposited time and other variable of electrodeposition process (e.g. nanoparticles composition). The effect of nanoparticles on thickness can be explained by the growth of the agglomerating particles in the layers that become bigger when higher amounts of particles are present (Leng et al., 2006).

In figure 2 SEM images of Ni/Al₂O₃ electrodeposition are displayed for five different alumina nanoparticles concentrations reaching to 100g/l.

Fig. 2. SEM images of Ni/Al₂O₃
As alumina was added to the electrolyte in increasing concentrations, a general refinement in the grain structure on the surface is observed. With addition of 5 g/l of alumina, the average size of the pyramids on the surface is clearly reduced (Gheorghies et al., 2006). There is also a reduction in the surface grain size to micrometer and sub micrometer grains. These results show that the surface morphology is greatly refined by the presence of alumina in the bath for the coatings deposited at 2 A.dm⁻².

The chemical analysis of electrodeposited layer with alumina nanoparticles has been estimated by EDAX method. The typical spectrum showing the chemical construction is presented in figure 3.

Fig. 3. EDAX spectrum of electrodeposited film with alumina nanoparticles

X-ray pattern from an electrodeposited film of nickel having a concentration of 10 % alumina nanoparticles in figure 4 is presented. Although EDAX spectra pointed out aluminum, only the characteristic peaks of nickel can be observed.

Fig. 4. X-ray diffraction pattern of electrodeposited nickel film with 10 % alumina nanoparticles

The thin films of nickel which were obtained with zirconia nanoparticles present in the electrolyte had an uniform white-silvery appearance. To obtain a reference for the determination of deposition efficiency, three pure nickel depositions were first conducted. In theory, there should have been deposited 8.21 g/dm², while experiments showed a
deposit of 7.8241 g/dm². Nickel weight deposited on the specimen was \( m_{\text{experimental}} = 0.3129 \) g and \( m_{\text{theoretical}} = 0.3284 \) g. Achieved efficiency was \( \eta = 95.30 \% \) i.e. an optimum deposition efficiency over 95%, typical for nickel depositions in an electrolytic bath of sulfate-chloride; in a Watt’s bath, 97.5% efficiency is obtained. Average weight of nickel with \( \text{ZrO}_2 \) deposited on the specimen is \( m_{\text{experimental}} = 0.2822 \) g. From \( m_{\text{theoretical}} \) and \( m_{\text{experimental}} \), efficiency can be deduced as \( \eta = 85.94 \% \).

Pure nickel depositions were obtained with an efficiency of more than 95.30%. On the other hand, in the experiments performed for composite depositions, a smaller efficiency was achieved due to the presence of \( \text{ZrO}_2 \) particles. One possible explanation is that in the paths followed by the \( \text{Ni}^{2+} \) ions to the cathode and that of the anions to the anode, \( \text{ZrO}_2 \) particles in the suspension may slow the nickel reduction process. Moreover, \( \text{ZrO}_2 \) particles can be found in the deposits, and there is an equilibrium between the forces keeping the particles down in the deposition and those existing in the suspension. This situation is not yet fully understood for a composite deposition mechanism.

4. Corrosion tests

Corrosion tests have been performed for composite coating specimens of \( \text{Ni}/\text{ZrO}_2 \) in three different types of solvents: \( \text{NaCl} \) 3%, \( \text{Na}_2\text{SO}_4 \) 0.1M and \( \text{H}_2\text{SO}_4 \) 0.1N. The results were compared with depositions of metallurgical nickel. The \( \text{Na}_2\text{SO}_4 \) 0.1 M solution is an electrolyte who has the advantage of being inert over most of the other tested materials, and the 0.1 M concentration ensures the appropriate conductivity for the three electrochemical studies that were performed: polarization curve, EIS spectroscopic impedance, and Mott-Schottky spectroscopic impedance (Yoo et al., 2006).

Previously, we isolated with nylon (polytetrafluoroethylene) the surface not subjected to electrochemical tests. Out of the deposited coating \( \text{Ni/ZrO}_2 \) area of 4 cm², an area of 0.5–1 cm² was reserved for the electrochemical experiments, polarization curves and spectroscopic impedance.

The electrochemical cell used for the electrochemical tests consisted of a glass recipient with a cap having a series of apertures through which we inserted the solution to be analyzed, the working electrode [deposition specimen obtained on the copper support], the auxiliary electrode [helical platinum (Pt) wire] and the referential electrode [horn mercury electrode \( \text{Hg/HgCl}_2\text{sat.} (\varepsilon = 0.234 \text{ V}) \)]. The solution was stirred by introducing a small magnet covered by a nylon or glass layer, which was then moved a magnetic stirrer.

Nickel specimens with zirconium oxide particles have been studied against pure nickel specimens. Initially, polarization curves were achieved in the previously mentioned electrolyte solutions (\( \text{NaCl} \) 3%, \( \text{Na}_2\text{SO}_4 \) 0.1M and \( \text{H}_2\text{SO}_4 \) 0.1N). Then we observed the behavior of the \( \text{Ni/ZrO}_2 \) depositions and that of the metallurgical nickel specimen.

The working circuit consisted of: referential electrode: horn mercury, auxiliary electrode: platinum and working electrode: deposition in nickel matrix. This circuit was connected to a computer which recorded the experimental data. The polarization curves \( i = f (E) \) were obtained in the following conditions: voltage 0: -500 mV; voltage 1: +500 mV; voltage 2: +1000 mV; sweeping speed (rate) \( v = 150 \text{ mV/min} \); number of cycles: 1, minimum current: -50 mA and maximum current: +50 mA. Figures 5-7 contain these polarization curves, and the corresponding numerical values are are synthetically reported in Table 2.
Table 2. Experimental data obtained from Polarization curves

<table>
<thead>
<tr>
<th></th>
<th>Ni</th>
<th>Ni/ZrO&lt;sub&gt;2&lt;/sub&gt;</th>
<th>Ni</th>
<th>Ni/ZrO&lt;sub&gt;2&lt;/sub&gt;</th>
<th>Ni</th>
<th>Ni/ZrO&lt;sub&gt;2&lt;/sub&gt;</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Na&lt;sub&gt;2&lt;/sub&gt;SO&lt;sub&gt;4&lt;/sub&gt; 0.1 M</td>
<td>NaCl 3%</td>
<td>H&lt;sub&gt;2&lt;/sub&gt;SO&lt;sub&gt;4&lt;/sub&gt; 0.1 N</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>E (i=0) (mV)</td>
<td>-321.1</td>
<td>-131.3</td>
<td>-237.1</td>
<td>-232.2</td>
<td>-257.9</td>
<td>-257.9</td>
</tr>
<tr>
<td>R&lt;sub&gt;p&lt;/sub&gt; (kΩ·cm&lt;sup&gt;2&lt;/sup&gt;)</td>
<td>16.41</td>
<td>104.54</td>
<td>7.85</td>
<td>20.98</td>
<td>126.63</td>
<td>126.63</td>
</tr>
<tr>
<td>i&lt;sub&gt;cor&lt;/sub&gt; (µA/cm&lt;sup&gt;2&lt;/sup&gt;)</td>
<td>0.9583</td>
<td>0.0693</td>
<td>1.299</td>
<td>0.229</td>
<td>0.0909</td>
<td>0.0909</td>
</tr>
<tr>
<td>v&lt;sub&gt;cor&lt;/sub&gt; (mm/year)</td>
<td>0.013</td>
<td>0.001</td>
<td>0.018</td>
<td>0.003</td>
<td>1.243</td>
<td>1.243</td>
</tr>
<tr>
<td>A (cm&lt;sup&gt;2&lt;/sup&gt;)</td>
<td>7.9</td>
<td>0.6</td>
<td>8.69</td>
<td>0.72</td>
<td>8.69</td>
<td>0.54</td>
</tr>
</tbody>
</table>

Key: E – voltage; i<sub>cor</sub> – corrosion intensity; R<sub>p</sub> – polarization resistance; v<sub>cor</sub> – corrosion rate; A – surface area

Fig. 5. Polarization curves: a) Ni in NaCl 3% solution, b) Ni/ZrO<sub>2</sub> in NaCl 3% solution

Fig. 6. Polarization curve: a) Ni in Na<sub>2</sub>SO<sub>4</sub> 0.1 M solution, b) Ni/ZrO<sub>2</sub> in Na<sub>2</sub>SO<sub>4</sub> 0.1 M solution
The obtained curves and the rates of corrosion indicate that the voltage is shifted to higher positive values for composite coatings of Ni/ZrO$_2$ (-232.2 mV for NaCl 3% solution; -131.3 mV for Na$_2$SO$_4$ 0.1M solution) against the metallurgical nickel (-237.1 mV for NaCl 3% solution; -321.1 mV for Na$_2$SO$_4$ 0.1M solution) and against the initial voltage, – 500 mV. In H$_2$SO$_4$ 0.1N solution, the voltage is found as being the same (-257.9 mV). The highest positive potential (-131.3 mV) was obtained for composite coatings of Ni/ZrO$_2$ in Na$_2$SO$_4$ 0.1 M electrolyte. A significant decrease in voltage occurs for the Ni/ZrO$_2$ specimens in Na$_2$SO$_4$ 0.1 M electrolyte, of approximately 200mV decrease. For the other electrolytes, no signification changes between the composite depositions and pure Ni were recorded.

The highest change in polarization resistance compared with pure Ni is obtained for Ni/ZrO$_2$ composite deposition in a Na$_2$SO$_4$ 0.1 M electrolyte. Correlated with this parameter, the corrosion intensity is the lowest on the same specimens, respectively 0.0693 ($\mu$A/cm$^2$) for a polarization resistance of 104.54 (Kohm·cm$^2$). The higher corrosion resistance and smaller the corrosion intensity are, the more resistant is the specimen to the destruction process.

In table 3 the corrosion rates are listed, expressed in mm/year. The lowest value was obtained for Ni/ZrO$_2$ composite deposition in Na$_2$SO$_4$ 0.1 M electrolyte (0.001 mm/year) and the second lowest one for NaCl 3% (0.003 mm/year).

<table>
<thead>
<tr>
<th>t (min.)</th>
<th>10</th>
<th>45</th>
<th>60</th>
<th>70</th>
<th>85</th>
<th>90</th>
<th>120</th>
<th>140</th>
</tr>
</thead>
<tbody>
<tr>
<td>E (V)</td>
<td>0.18</td>
<td>0.15</td>
<td>0.15</td>
<td>0.15</td>
<td>0.14</td>
<td>0.13</td>
<td>0.11</td>
<td>0.1</td>
</tr>
<tr>
<td>t (min.)</td>
<td>180</td>
<td>200</td>
<td>240</td>
<td>1440</td>
<td>2670</td>
<td>2735</td>
<td>2790</td>
<td>2820</td>
</tr>
<tr>
<td>E (V)</td>
<td>0.09</td>
<td>0.09</td>
<td>0.08</td>
<td>0.09</td>
<td>0.1</td>
<td>0.09</td>
<td>0.02</td>
<td>0</td>
</tr>
</tbody>
</table>

Table 3. Experimental data on Spectroscopic Impedance research

In the H$_2$SO$_4$ 0.1 N electrolyte, which is highly acidic, the parameters for specimens studied by comparison are identical, thus polarization curve research in this electrolyte does not provide analytical information.

In conclusion, the determination of the polarization curve must be performed in a proper electrolyte, to maximize the amount of information useful for research. For the studied specimens it was proved that Na$_2$SO$_4$, which is an inert electrolyte which resulted from a
tough acid and a tough base, is the most appropriate for the study of polarization curves. Ni/ZrO$_2$ composite deposition specimens show significantly improved parameters ($R_p$ and $i_{corr}$) compared with metallurgical Ni.

In figure 8, the overlapping of two polarization curves is shown: Ni/ZrO$_2$ in Na$_2$SO$_4$ 0.1 M solution and Ni/ZrO$_2$ in NaCl 3% solution. The two curves cross at: on voltage $E$ (-300 mV, -200 mV) and a corrosion rate $i_{corr} = 0$ $\mu$A/cm$^2$.

![Fig. 8. Polarization curves – Overlapping: Ni/ZrO$_2$ in Na$_2$SO$_4$ 0.1 M solution (1), Ni/ZrO$_2$ in NaCl 3% solution (2)](image)

In figure 9, the polarization curve is shown for nickel and Ni/ZrO$_2$ specimens in H$_2$SO$_4$ 0.1 N solution. The curve for nickel has a maximum peak at a voltage $E$ (-7 mV, 14 mV) and a corrosion rate $i_{corr}$ (2.150 $\mu$A/cm$^2$, 2.154 $\mu$A/cm$^2$). For Ni/ZrO$_2$ two maximum peaks are present at a voltage $E_1$ (-65 mV, -55 mV), a corrosion rate $i_{corr1}$ (4 $\mu$A/cm$^2$, 4.2 $\mu$A/cm$^2$), and at a voltage $E_2$ (80 mV, 100 mV), with a corrosion rate $i_{corr2}$ (2.3 $\mu$A/cm$^2$, 2.5 $\mu$A/cm$^2$).

In addition, we juxtaposed the polarization curves for Ni/ZrO$_2$ in H$_2$SO$_4$ 0.1 N solution (1), and Ni in H$_2$SO$_4$ 0.1 N solution (2). Both curves have a peak in the same voltage range: $E$ (-255 mV, 200 mV).

![Fig. 9. Polarization curves: Ni/ZrO$_2$ in H$_2$SO$_4$ 0.1 N solution (1), Ni in H$_2$SO$_4$ 0.1 N solution (2) – Overlapping](image)
For composite coatings like nickel – zirconium oxide, compared to nickel coatings, polarization curves have almost the same rates, but shifted to an increased voltage, proving that these composite coatings have better resistance to corrosion.

The corrosion protection can be attributed to the presence of ZrO$_2$ particles in nickel matrix, because their presence on the metal surface creates a barrier for oxygen reduction. In solutions, the composites are not stable. It is possible to selectively dissolve the metallic matrix or the disperse phase or both (matrix-disperse phase).

Corrosion processes are essentially electrochemical nature processes and voltage and current parameters can be accurately measured with modern equipment. For the corrosion study, polarization resistances can be evaluated from spectro-electrochemical impedance data (EIS) in a large frequency range ($10^5 - 10^{-3}$ Hz). A voltage change indicates a corresponding change of intermediate species concentration.

The spectroscopic impedance measurements were performed on composite specimens, nickel with zirconium oxide (Ni/ZrO$_2$) particles in Na$_2$SO$_4$ solution, as working electrolyte for the electro-chemical cell. This way, the behavior of the layer deposited in the electrolytic solution was traced during a period of time, to evaluate the parameters.

The working equipment contains a two component circuits: the main and secondary circuits. The main circuit consists of: referential electrode: horn mercury (connected to white color); auxiliary electrode: platinum (connected to red and orange colors) and working electrode: specimen (connected to green and blue colors). The secondary circuit is realized by a salt bridge connecting the referential electrode to the working electrode (Hamann et al., 1998). The salt bridge prevents contamination of saturated KCl solution from the horn mercury electrode with impurities coming from the solution to be analyzed. To measure the voltage in horn mercury, a voltmeter was introduced in the circuit, with a lug to referential electrode and one to the working one. This circuit is connected to computer and data for electrochemical analysis are recorded.

Specimens undertaking the experiments have been evaluated for certain time spans. The value of voltmeter-measured voltage is reported during the entire electrochemical analysis. Results are rendered in table 3, and diagram $E= f(t)$ is rendered in figure 11. From the spectroscopic impedance measurements, an evaluation can be made by comparing the differences between the measuring voltage values depending on time, as presented in table 3. The voltages can provide insight into the strength of the coating.

From figure 10 shows that voltage changes with time, and a constant voltage drop is recorded from 180 mV to 0 mV during 47 hours. Additional data is presented in figures 11-

![Fig. 10. Voltage variation on time](www.intechopen.com)
12, rendered as Bode and Nyquist charts. Bode chart is usually useful to physicists, while Nyquist chart is preferred by chemists. The impedance measurements on various frequencies can provide full information on the electrochemical system, which gives a particular value to this technique (Hamann et al., 1998; Rusu et al. 2010).
Fig. 11. Representation of Impedance Spectroscopy (BODE Diagram) for the experimental system of Ni/ZrO$_2$ in Na$_2$SO$_4$ 0.1 M solution at $t = 0$ s(a), 1 h(b), 2 hrs(c), 3h(d), 4 hrs(e), 24h(f), 46 hrs(g), 47(h)

Figure 12 shows that Ni/ZrO$_2$ composite system has a high polarization resistance, with a maximum of 40 Kohm for a high frequency. After 46 hours Nyquiest diagram shows a small 300 ohm polarization resistance, and a small decrease of polarization resistance with time. This suggests that the presence of zirconium oxide in the deposition may cause load transfer, since this substance can act as activator for the cathode reduction process of the metal.

A specimen of Ni/ZrO$_2$ composite deposition was subjected to Mott Schottky approach, which is a variant of Spectroscopic Impedance. In this approach, behavior of voltage depending resistance and capacity is traced. The data we obtained is plotted in figures 13-15. At a voltage of ~100 mV the specimen has a high polarization resistance and the capacity is at a minimum of 0 mV, which explains the good properties of the specimen in the 0-100 mV range, and its corrosion resistance on higher voltages. The capacity decreases for the interval: $E \in (-500 \text{ mV}, 0 \text{ mV})$ and then increases for the interval $E \in (0 \text{ mV}, 500 \text{ mV})$. 
Fig. 12. Representation of Impedance Spectroscopy (Nyquist diagram) for the experimental system of Ni/ZrO$_2$ in Na$_2$SO$_4$ 0.1 M solution at $t = 0$ s (a), 1h (b), 2 hrs (c), 3 hrs (d), 4 hrs (e), 24 hrs (f), 46 hrs (g), 47 hrs (h).
Our experiments have shown that the Ni/ZrO₂ composite coatings resist better to corrosion, compared to metallurgical nickel depositions. The best corrosion protection is obtained when the layers have low capacity. The layer is less active, therefore more resistant to corrosion.

The specimens subjected to electrochemical studies were washed with plenty of distilled water and dried, and the raylon was subsequently removed from the coated surface (Rieger,
Thiemig et al. 2009). The specimens can be inspected with an electronic microscope to view potential alterations of the surface to be studied.

![Polarization curve and variation of capacity](image)

**Fig. 15.** Polarization curve (1) and variation of capacity (2) of nanocomposite thin films

### 5. Conclusions

This paper deals with the electrochemical preparation and study of Ni/Al₂O₃ and Ni/ZrO₂ nanocomposite thin layers on Inconel or cooper substratum. The comparison between the properties of composite coatings and metallurgical nickel coatings yielded conclusive results. Electrochemical processes offer an alternative way for obtaining composite coatings with unique properties, superior to those of constituent materials. More than that, the composite coatings can be obtained using affordable processes which offer precise control on its parameters. We determined the most relevant factors for the success of composite coatings with directed composition are the nature of constituents, and electrolyte and electrolysis conditions. For example, the chemical and physical reactions of Ni/ZrO₂ composite plating depend on the electrolyte, for each test solution used.

The study of polarization curves and electrochemical impedance offers useful information on the kinetics of chemical reactions on the electrode. The corrosion voltage has higher values for composite coatings of Ni/ZrO₂ in Na₂SO₄ 0.1 M solution, which is the most appropriate solution for studying the polarization curves. The 0.1 M Na₂SO₄ concentration has an appropriate conductivity for performing electrochemical tests. The physical and chemical properties (hardness, stability, wear and chemical resistance) of composite coatings are superior to those obtained by conventional procedures and recommend their usage in electronics, medicine, engineering and anti-corrosion protection.
Alumina and zirconia composite electrodepositions were done in a nickel matrix, and the result exhibited higher corrosion resistance than that of pure nickel. Additions of alumina nanoparticles with a particle size of 20 nm of 5 g/l and 10 g/l into nickel plating bath change the preferred growth direction of the electrodeposited nickel from \(<100>\) to \(<111>\). When alumina is added, the microstructure of nanocomposite coatings is different from that obtained using pure nickel. Moreover, deposition of zirconia in nickel metallic matrix improves anti-corrosion protection of layers. The obtained results are promising for developing new corrosion-resistant materials. They suggest that metal oxide nanoparticles coatings can be an effective option for surface protection, as it introduces a barrier against aggressive environment and metallic sub-layer. This approach is relatively new and warrants further research into the mechanisms that cause nickel-metal oxide composite coatings to improve corrosion resistance.

6. Acknowledgement

The authors thanks for the support of this work to T. Lempke and S. Steinhauser from Chemnitz University, Germany, and to C. Radovici and R. Banu from UPB Bucharest, as well as to G. Carac from Dunarea de Jos of Galati, Romania.

7. References


Advances in Nanocomposites - Synthesis, Characterization and Industrial Applications was conceived as a comprehensive reference volume on various aspects of functional nanocomposites for engineering technologies. The term functional nanocomposites signifies a wide area of polymer/material science and engineering, involving the design, synthesis and study of nanocomposites of increasing structural sophistication and complexity useful for a wide range of chemical, physicochemical and biological/biomedical processes. "Emerging technologies" are also broadly understood to include new technological developments, beginning at the forefront of conventional industrial practices and extending into anticipated and speculative industries of the future. The scope of the present book on nanocomposites and applications extends far beyond emerging technologies. This book presents 40 chapters organized in four parts systematically providing a wealth of new ideas in design, synthesis and study of sophisticated nanocomposite structures.

How to reference
In order to correctly reference this scholarly work, feel free to copy and paste the following:

© 2011 The Author(s). Licensee IntechOpen. This chapter is distributed under the terms of the Creative Commons Attribution-NonCommercial-ShareAlike-3.0 License, which permits use, distribution and reproduction for non-commercial purposes, provided the original is properly cited and derivative works building on this content are distributed under the same license.